

1. Project Aims

- Development** - Modify the in-house *OpenFOAM*-based Actuator Line Code to account for platform motions.
- Validation** - Validate simulation results against experimental force and wake data.
- Application** - Apply the method to explore the interaction between ambient turbulence and platform-motion-induced coherent structures.

2. Importance of Floating Offshore Wind Energy

- Access to deeper waters** - estimated 80% of all practical wind energy potential found in deeper waters⁴.
- Higher wind speeds** - Stronger and more consistent wind speeds allow for greater yield.
- Smaller seabed footprint** - Floating turbines do not require a monopile foundation.
- Increased complexity** - Platform design introduces complexity and design methods have not yet converged¹.
- Additional Unsteadiness** - Platform motions introduce unsteadiness into the wake.

⇒ Understanding the dynamic wake system poses a major challenge in FOWT farm optimisation and requires high-fidelity yet computationally affordable models. One such candidate model is the floating actuator line method.

3. Experimental Validation Case

- UNAFLOW² & NETTUNO³ experimental campaigns.
- 1:75 scaled 10MW version of the DTU-10MW turbine.
- 2.38m diameter rotor resulting in a (local/global) blockage of (48.7%/8.4%) in the POLIMI wind tunnel.
- Thrust, torque and wake measurements.
- Monochromatic platform motions in pitch, surge, yaw, roll, and sway.

4. Methodology

- Turbine** - Representation via actuator line method (fig. 1).
- Turbulence** - Ambient turbulence recreated via divergence free synthetic eddy method⁵. Flow field solved for using large eddy simulation with Smagorinsky model for subgrid stresses. See fig. 2.
- Blockage** - Boundary layers represented via wall models ($y^+ \approx 180$).
- Solver** - Discretised using the finite volume method with cell size $\Delta = D/120$. Solved using PIMPLE algorithm. Mesh contains approximately $15 \cdot 10^6$ cells.

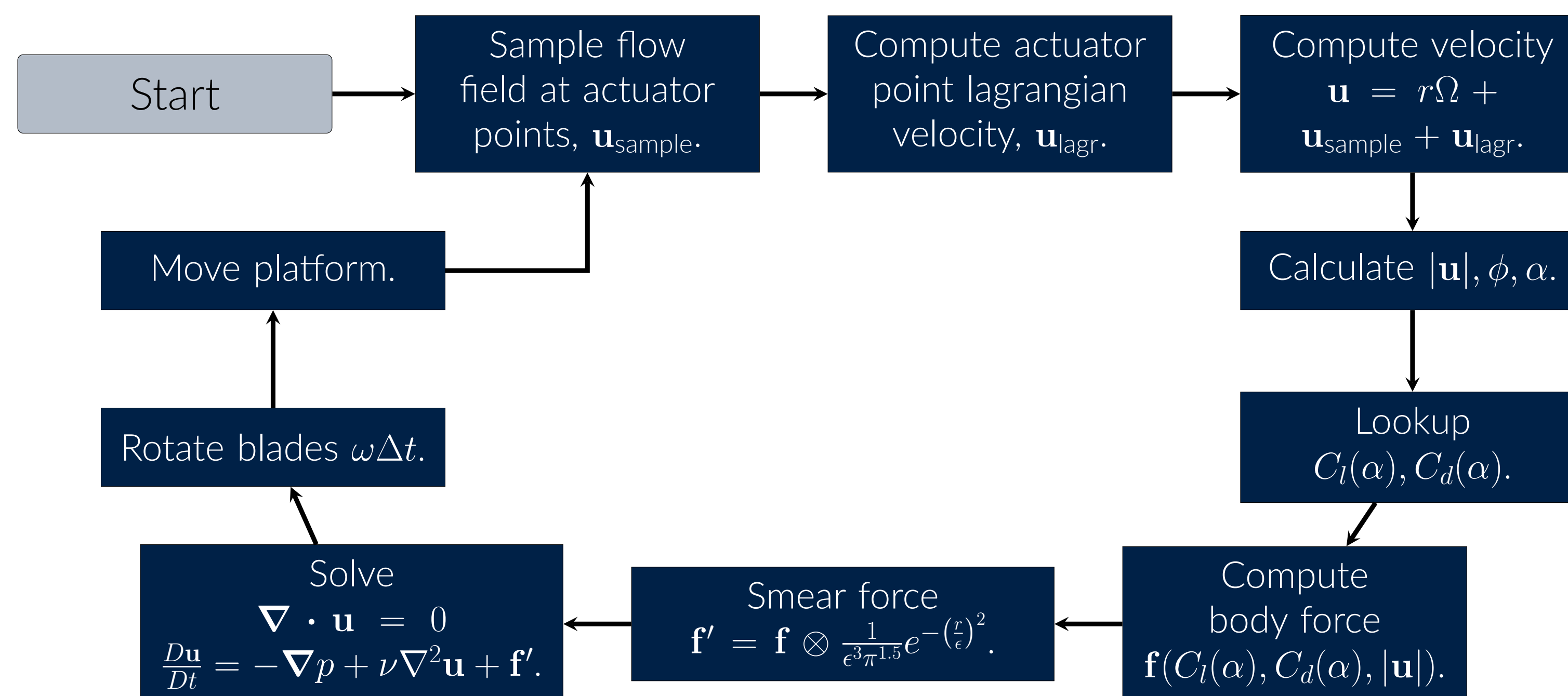


Figure 1. Modified actuator line method procedure.

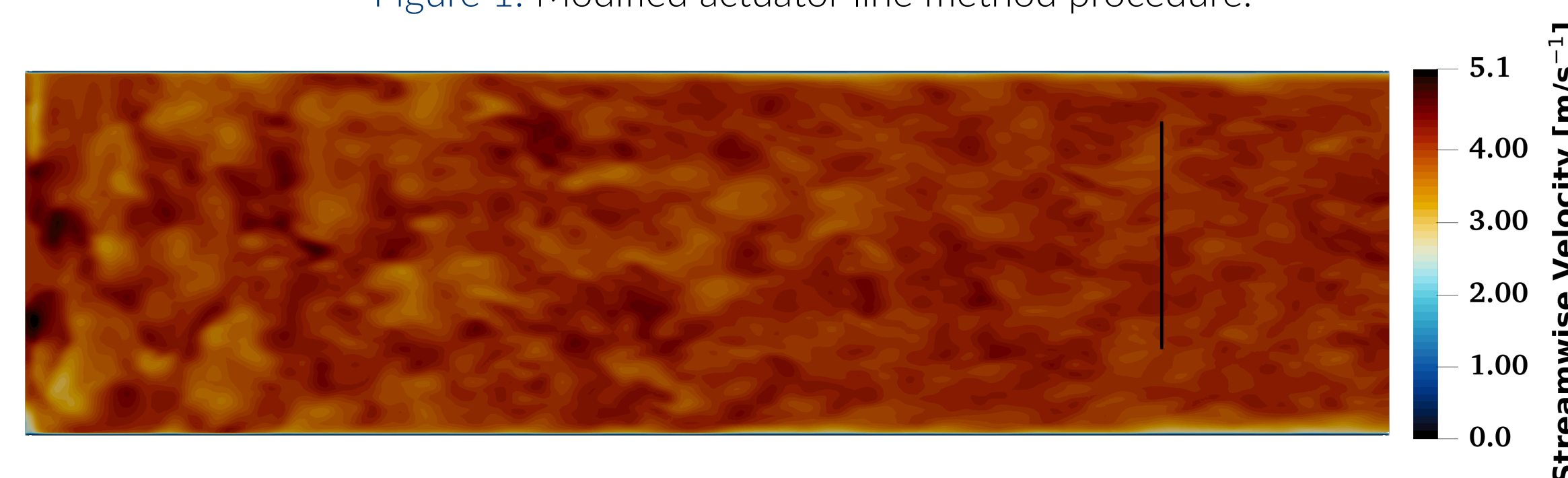


Figure 2. Inlet turbulence plotted over a streamwise-vertical plane. The rotor plane is labeled with a black line.

5. Results

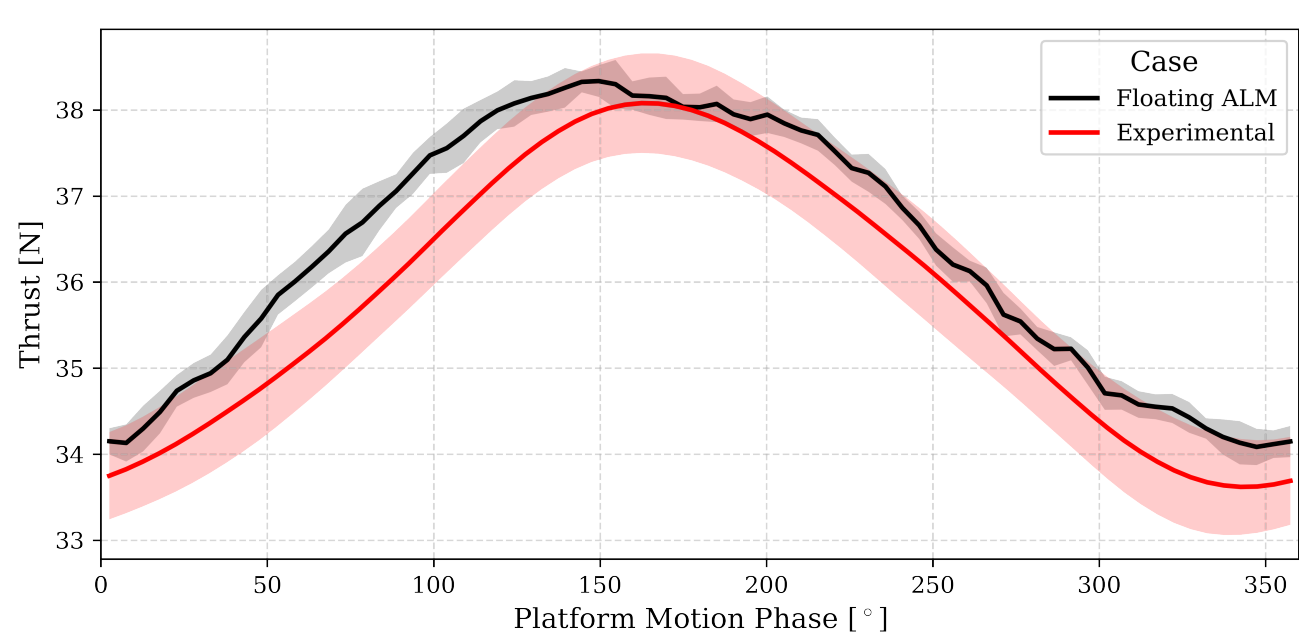


Figure 3. Phase averaged thrust variation of a pitching turbine with harmonic platform motions described by $A = 1.3^\circ$, $f = 1\text{Hz}$.

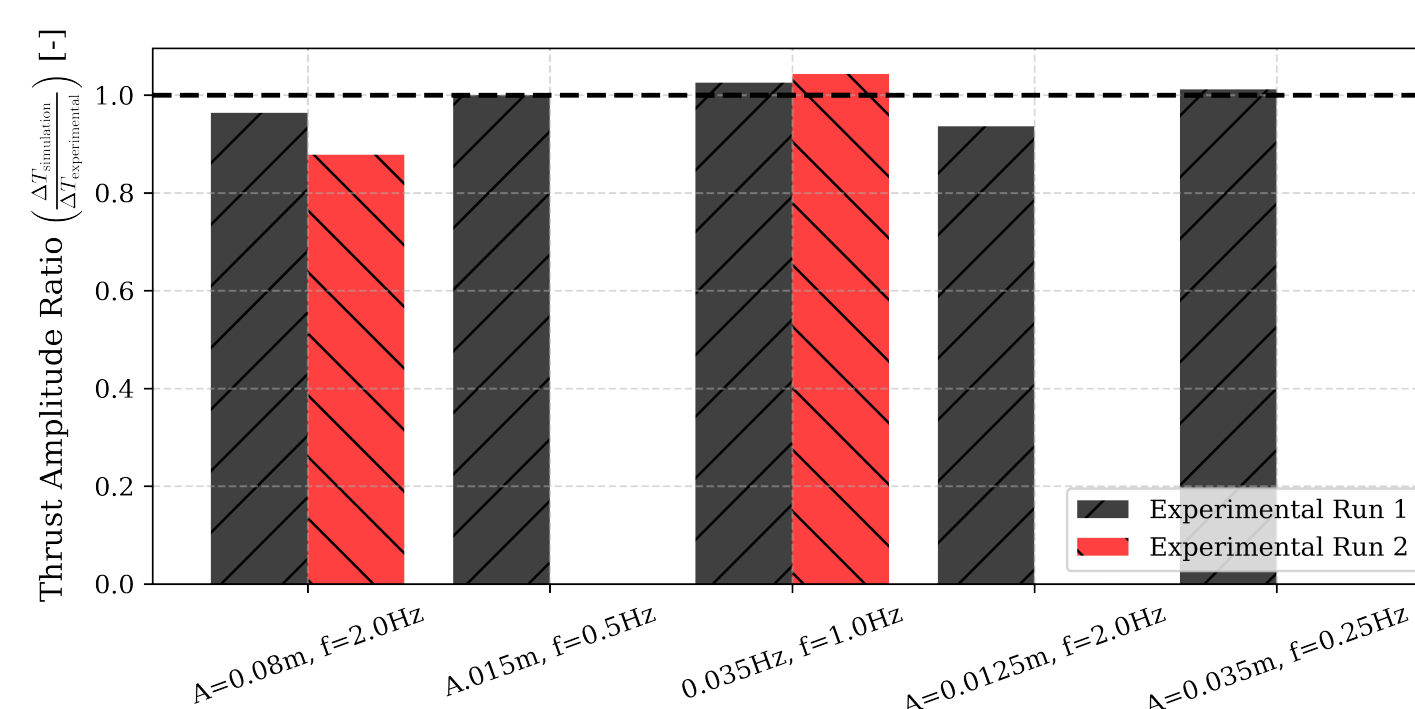


Figure 5. Comparison thrust variation for surging cases. Simulation thrust variation is normalised by the experimental thrust variation.

Rotor Forces:

- Rotor thrust oscillation amplitude shows good agreement across multiple cases with varying dynamics.

Rotor Wake:

- Phase-averaged wake results agree well within the outer wake region ($r/R > 0.7$). However, the absence of nacelle representation leads to an overprediction of the streamwise velocity near the hub.
- Q -Criterion contour shows how the actuator line method is able to resolve the complex wake structure and therefore any platform-induced interactions.

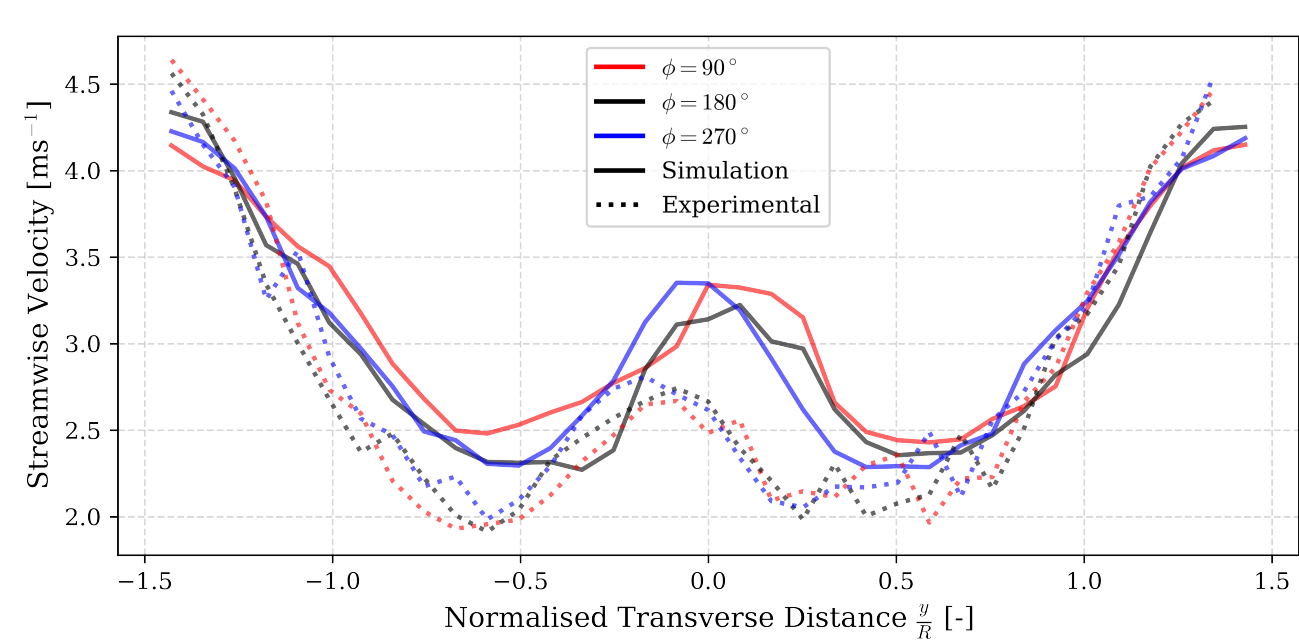


Figure 4. Horizontal phase averaged wake profile of a pitching turbine with harmonic platform motions described by $A = 1.3^\circ$, $f = 1\text{Hz}$.

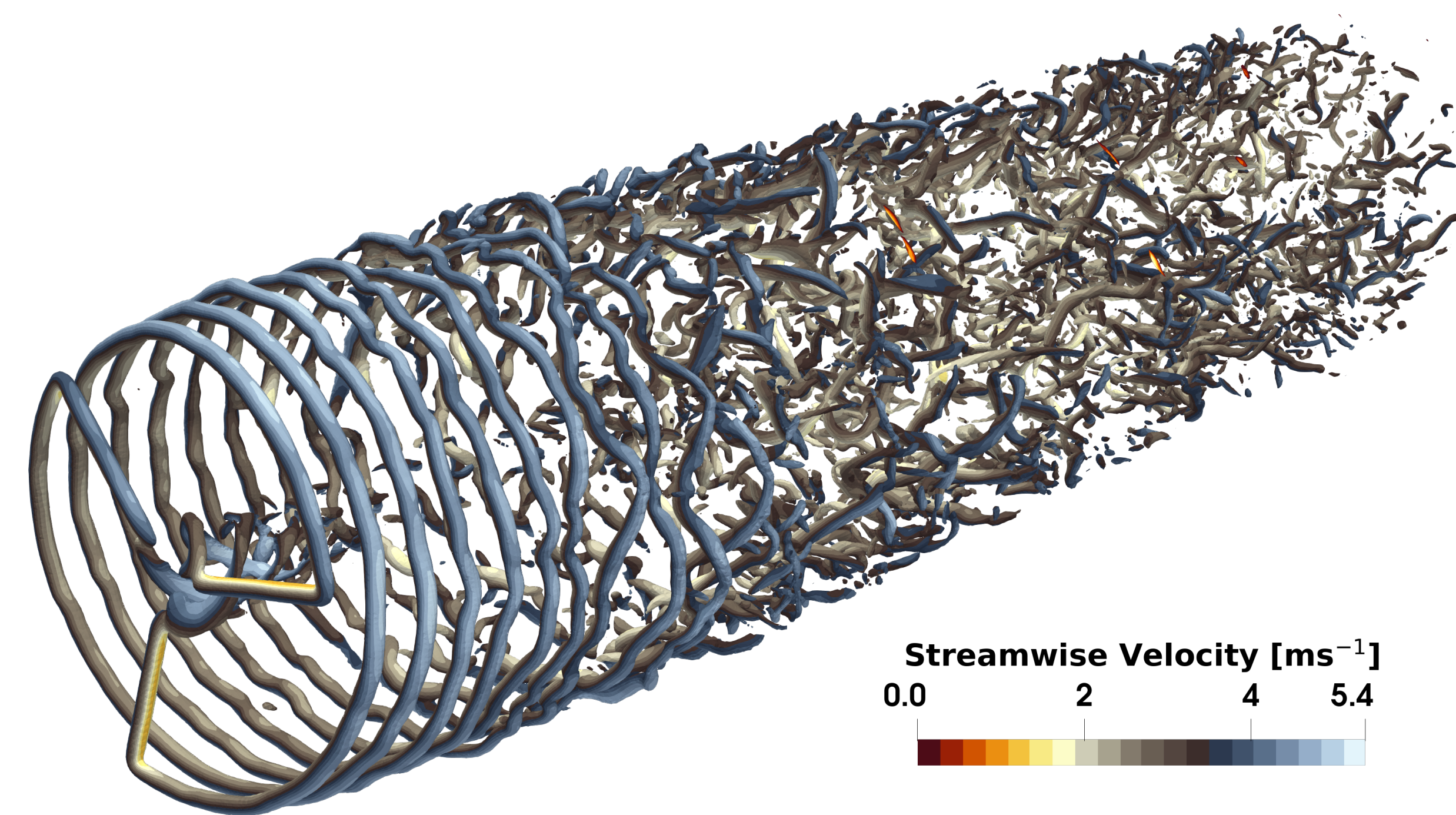


Figure 6. Q -criterion contour plot of a pitching turbine with harmonic platform motions described by $A = 1.3^\circ$, $f = 1\text{Hz}$.

6. Conclusions / Key Takeaways

- Experimental and numerical results show good agreement in rotor force and wake prediction.
- The floating actuator line method is able to produce accurate results without explicit blade representation resulting in large computational savings.
- Turbulence produced by the divergence-free synthetic eddy method is able to reproduce experimental conditions.
- Future work:** Actuator-based representation of floating towers and nacelles, characterisation of complex floating-motion-induced wake instabilities, comparative study of floating actuator line and disc wakes.

Bibliography

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